

1 **4.7 NOISE**

2 This analysis is based on a Community Noise Technical Study (attached as Appendix J)
3 prepared for the project by URS, as well as Environmental Documents prepared for the Tajiguas
4 Landfill Project (listed in Section 1.4.2).

5 **4.7.1 Setting**

6 4.7.1.1 Characteristics of Noise

7 The Santa Barbara County Comprehensive Plan Noise Element provides a
8 thorough background discussion of noise and its effects on human health and
9 quality of life, as well as a discussion of noise measurement descriptors used in
10 establishing noise standards. The following paragraphs present a brief
11 summary of the terms and standards used in community noise analysis.

12 Noise levels are measured in a logarithmic scale (with units of decibels) in a
13 way that duplicates the frequency sensitivity of the human ear (the “A” scale),
14 with the abbreviation of dBA. Typically, noise levels in rural and suburban
15 areas range from low values between 35 to 45 dBA, up to levels between 65 to
16 75 dBA, which may be associated with locations near highways or arterial
17 roadways. Normal human speech becomes nearly inaudible when background
18 noise levels are around 60 to 65 dBA. Noise levels in close proximity to
19 machinery such as lawn mowers or heavy trucks or earth moving equipment,
20 may reach 95 to 100 dBA.

21 Often noise levels vary over short periods of time and it is necessary to use a
22 single dBA value to represent such changing noise levels. The single value,
23 which may be measured or computed to represent the same amount of
24 acoustic energy transmitted by a varying noise level, is called the Equivalent
25 Noise Level (Leq) and must always be associated with the defined time period
26 over which it applies. It is common to express Leq values for one-hour time
27 periods, but shorter and longer periods might also be specified.

28 Many standards and guidelines for acceptable noise levels are based on 24-
29 hour periods. For these types of standards the hourly Leq values are
30 determined for different portions of the day, and then “penalty” dBA values are
31 added to the noise levels during the evening and/or nighttime periods to
32 account for the added nuisance of noise during these periods. Two common
33 noise descriptors of this type are the Day-Night Average Noise Level (Ldn) and
34 the Community Noise Equivalent Level (CNEL). The Ldn includes a 10 dBA
35 addition during the nighttime hours (10:00 p.m. to 7:00 a.m.). Ldn is calculated
36 from day and night noise values as follows:

1
$$Ldn = 10\log_{10}[(15/24)(10^{Ld/10}) + (9/24)(10^{(Ln+10)/10})]$$

2 Where:

3 Ldn = Day-Night Average Noise Level, dBA

4 Ld = Equivalent Noise Level during Daytime, 15 hours from 7:00 a.m. to
5 10:00 p.m.

6 Ln = Equivalent Noise Level during Nighttime, 9 hours from 10:00 p.m. to
7 7:00 a.m.

8 The CNEL is similar to Ldn, but also includes a 5 dBA addition during the
9 evening hours (7:00 p.m. to 10:00 p.m.). The numerical difference between
10 Ldn and CNEL values is small. Many publications, including the Santa Barbara
11 County Comprehensive Plan Noise Element, use the two terms
12 interchangeably.

13 Most noise levels are measured or computed to show their value at a
14 standardized distance from the noise source, commonly 50 feet. Whenever a
15 source noise level is measured or cited, the distance to the source should
16 always be specified or clearly known. As the distance to the receiver location
17 becomes greater, the noise level decreases in a logarithmic fashion. For a
18 doubling of the distance from most point noise sources, the dBA value of the
19 noise will decrease by 6 dBA. For a perfect line source, the decrease amounts
20 to only 3 dBA for each doubling of distance. Depending on their traffic volume
21 and geometry, roadways are treated as either a line source or as something
22 between a point and a line source, with the rate of decrease usually estimated
23 as either 3.0 dBA (line source) or 3.5 to 4.5 dBA (between a line and a point
24 source) for each doubling distance.

25 Noise levels are often summarized graphically by showing contours, which are
26 lines depicting equal noise values associated with a particular source (either a
27 single source, or an aggregate of multiple sources from one or more geographic
28 locations). For instance, a single noise level contour might show where 60 dB
29 is expected with respect to noise emission from a source; or, multiple contours
30 showing a range of dB values, often in decrements of 5 dB, could illustrate how
31 sound propagates away from that source and how it attenuates with distance.

32 Noise contours superimposed on an aerial photograph or map of noise-
33 sensitive land uses can help show where noise level exposure may exceed an
34 allowable threshold. Santa Barbara County considers the following as noise-
35 sensitive land uses:

- 36 • Residential, including single and multifamily dwellings, mobile home
37 parks, dormitories, and similar uses.
- 38 • Transient lodging, including hotels, motels, and similar uses.

- Hospitals, nursing homes, convalescent hospitals, and other facilities for long-term medical care.
- Public or private educational facilities, libraries, churches, and places of public assembly.

4.7.1.2 Characteristics of Ground-borne Vibration and Noise

In contrast to airborne noise, ground-borne vibration is not a common environmental problem. It is unusual for vibration from sources such as buses and trucks to be perceptible, even in locations close to major roads. Some common sources of ground-borne vibration are trains, buses on rough roads, and construction activities such as blasting, pile-driving and operating heavy earth-moving equipment.

The effects of ground-borne vibration include detectable movement of the building floors, rattling of windows, shaking of items on shelves or hanging on walls, and rumbling sounds. In extreme cases, the vibration can cause damage to buildings. Building damage is not a factor for most projects, with the occasional exception of blasting and pile-driving during construction. Annoyance from vibration often occurs when the vibration exceeds the threshold of perception by only a small margin. A vibration level that causes annoyance would be well below the damage threshold for normal buildings.

Vibration is an oscillatory motion which can be described in terms of the displacement, velocity, or acceleration. Because the motion is oscillatory, there is no net movement of the vibration element and the average of any of the motion descriptors is zero. Displacement is the easiest descriptor to understand. For a vibrating floor, the displacement is simply the distance that a point on the floor moves away from its static position. The velocity represents the instantaneous speed of the floor movement and acceleration is the rate of change of the speed. The peak particle velocity (PPV) is defined as the maximum instantaneous positive or negative peak of the vibration signal. PPV is often used in monitoring of blasting vibration since it is related to the stresses that are experienced by buildings.

4.7.1.3 Noise Sources in the Project Area

Noise sources in the project vicinity include U.S. Highway 101, Union Pacific Railroad operations, and existing operations at the Tajiguas Landfill. The Santa Barbara County Comprehensive Plan Noise Element estimates that the 60 dBA Ldn noise contour associated with U.S. Highway 101 in the project vicinity is about 250 feet from the centerline of the outer travel lane. This means that any residences within this distance from the highway would be subject to noise levels at or above 60 dBA Ldn.

1 Along the Union Pacific Railroad tracks, at a distance of 100 feet from the
2 tracks, the maximum noise levels from passing trains are 96 dBA to 100 dBA.
3 At this same distance, the Santa Barbara County Comprehensive Plan Noise
4 Element estimates noise levels are between 70 and 75 dBA CNEL, and the 65
5 dBA CNEL contour is estimated to be about 150 feet from the tracks.

6 The Tajiguas Landfill is currently permitted to receive up to 1,500 tons per day
7 of solid waste. Waste is brought to the landfill in large trucks and placed in
8 prepared disposal cells with large tracked tractors (D9 dozers) and dual-engine
9 scrapers. This equipment is also used in construction operations to obtain fill
10 material, to prepare waste disposal areas and to construct drainage and other
11 improvements within the landfill. Noise levels from these existing operations
12 have been assessed in the Tajiguas Landfill Expansion Project EIR (Section
13 4.7.2.2), and revised based on the modified waste footprint as described in the
14 Tajiguas Landfill Reconfiguration and Baron Ranch Restoration Project SEIR
15 (see Section 4.7.2.3).

16 4.7.1.4 Noise Measurements

17 As part of the Community Noise Technical Study prepared for the project, noise
18 levels were measured at two locations on April 4, 2013:

- 19 • Calle Real near the landfill, 100 feet north of the centerline of the U.S.
20 Highway 101 northbound lanes (9:56 – 10:06 a.m.);
- 21 • Tajiguas Landfill, 65 feet northwest of the landfill gas power plant (9:44 –
22 9:48 a.m.).

23 The Leq noise level measured along Calle Real was 66.7 dBA, while the Leq
24 noise level measured at the landfill was 75.8 dBA. Using the 75.8 dBA as a
25 reference level, and after applying only geometric divergence attenuation, an
26 extrapolated Leq of 60 dBA would be expected at a distance of 420 feet, which
27 after conversion to the CNEL metric becomes 66 dBA and agrees (within 1 dBA
28 CNEL) with the estimate of noise levels associated with Tajiguas Landfill
29 operations provided in the Landfill Reconfiguration Project SEIR (see Section
30 4.7.2.3).

31 4.7.1.5 Regulatory Setting

32 **Federal**

33 The U.S. Environmental Protection Agency has established maximum noise
34 level standards for a variety of vehicles and equipment (see 40 CFR Part 201).
35 For on-highway medium and heavy duty trucks, the applicable standards are in
36 Part 205, and require that all such vehicles manufactured after January 1, 1988,
37 have a maximum noise level of no more than 80 dBA at 50 feet under specified
38 conditions of acceleration and other measurement procedures.

1 The Federal Department of Transportation has standards and guidelines for
2 federally funded transportation projects such as highways, rail transit, and
3 airports. The regulations and procedures related to highways are found at 23
4 CCR Part 772, which applies to programs of the Federal Highway
5 Administration (FHWA). The FHWA developed the Traffic Noise Model, which
6 was used to estimate traffic noise for this project. Noise abatement criteria for
7 residential areas used in federal projects is based on the highest one-hour Leq,
8 and is 67 dBA. Other standards and procedures are defined in the regulations
9 to establish a uniform review system and approach to mitigating traffic noise
10 impacts.

11 For all motor vehicles (trucks and heavy equipment) used at off-highway job
12 sites, federal regulations require backup or reverse signal alarms that are
13 audible above the surrounding noise level (29 CFR 1626.601).

14 There are no specific federal laws related to allowable community noise levels.
15 However, residential projects that rely on federal Housing and Urban
16 Development (HUD) financing must meet exterior noise guidelines established
17 by HUD. HUD and other federal guidelines commonly use a 65 dBA CNEL as
18 the maximum noise level compatible with residential uses.

19 **California**

20 The California Government Code (Section 65302(f)(1)) requires the inclusion of
21 a Noise Element within the General Plan, the contents of which are specified by
22 the Governor's Office of Planning and Research as part of their General Plan
23 Guidelines. California building standards that relate to noise levels and
24 required insulation provisions for residential uses are found in the state Building
25 Code (24 CCR Chapter 12), but apply only to multi-family residential structures.

26 Caltrans prepares traffic noise analyses in a manner that implements the
27 FHWA regulations at 23 CFR Part 772, described in the preceding section. For
28 off-highway vehicles capable of hauling or carrying more than 2.5 cubic yards of
29 material, automatic backup alarms must be provided that can be heard for at
30 least 200 feet in all directions (8 CCR 1592(a)).

31 **Santa Barbara County**

32 The Santa Barbara County Land Use and Development Code does not have a
33 separate noise section. Instead, noise performance standards are set forth in
34 the various zones defined in the code. The Tajiguas Landfill, however, is in an
35 area with the U-Unlimited Agriculture zone, for which there is no specific noise
36 performance standard. The County Noise Ordinance (Section 40 of the County
37 Code) prohibits excessive noise in all areas between the hours of 10:00 p.m.
38 and 7:00 a.m., but does not set forth any other quantitative restrictions.
39 Applicable noise criteria to be used in assessing potential noise impacts are
40 found in the County's Comprehensive Plan Noise Element and in the
41 Environmental Thresholds and Guidelines Manual (see Section 4.7.2.1).

1 A Draft Gaviota Coast Plan was developed by the County Planning and
2 Development Department and released in February 2013 (revised in December
3 2013 as the Board of Supervisors Initiation Draft). The Tajiguas Landfill,
4 including the project site is located within the planning area. The Gaviota Coast
5 Plan would update the County Comprehensive Plan and Coastal Land Use
6 Plan, and provide policy direction for land use issues. The Plan does not
7 include any policies related to noise, but acknowledges that development of
8 new noise-sensitive land uses may be affected by noise generated by Union
9 Pacific Railroad and U.S. Highway 101 operations. Planning Commission
10 hearings were conducted from June through September 2013 to solicit public
11 input. As of June 2014, the Gaviota Coast Plan has not been adopted.

12 **4.7.2 Impact Analysis and Mitigation Measures**

13 4.7.2.1 Thresholds of Significance

14 **State CEQA Guidelines**

15 The State CEQA Guidelines (14 CCR Chapter 3, Appendix G) suggest that a
16 project may have a significant impact with respect to noise if it results in any of
17 the following:

- 18 • Exposure of persons to or generation of noise levels in excess of
19 standards established in the local general plan or noise ordinance, or
20 applicable standards of other agencies;
- 21 • Exposure of persons to or generation of excessive ground-borne vibration
22 or ground-borne noise levels;
- 23 • A substantial permanent increase in ambient noise levels in the project
24 vicinity above levels existing without the project; and,
- 25 • A substantial temporary or periodic increase in ambient noise levels in the
26 project vicinity above levels existing without the project.

27 **Santa Barbara County Thresholds**

28 The Santa Barbara County Environmental Thresholds and Guidelines Manual
29 includes several criteria used to define significant noise impacts:

- 30 a. A proposed development that would generate noise levels in excess of 65
31 dBA CNEL and could affect sensitive receptors would generally be
32 presumed to have a significant impact.
- 33 b. Outdoor living areas of noise-sensitive uses that are subject to noise
34 levels in excess of 65 dBA CNEL would generally be presumed to be
35 significantly impacted by ambient noise.
- 36 c. A significant impact would also generally occur where interior noise levels
37 cannot be reduced to 45 dBA CNEL or less.

- 1 d. A project will generally have a significant effect on the environment if it
2 will increase substantially the ambient noise levels for noise-sensitive
3 receptors adjoining areas. Per item a., this may generally be presumed
4 when ambient noise levels affecting sensitive receptors are increased to
5 65 dBA CNEL or more. However, a significant effect may also occur
6 when ambient noise levels affecting sensitive receptors increase
7 substantially but remain less than 65 dBA CNEL, as determined on a
8 case-by-case level.
- 9 e. Noise from grading and construction activity proposed within 1,600 feet of
10 sensitive receptors, including schools, residential development,
11 commercial lodging facilities, hospitals or care facilities, would generally
12 result in a potentially significant impact. According to EPA guidelines, the
13 average construction noise is 95 dBA at a 50 foot distance from the
14 source. A 6 dB drop occurs with a doubling of the distance from the
15 source. Therefore, locations within 1,600 feet of the construction site may
16 be affected by noise levels over 65 dBA.

17 **Caltrans**

18 The County Environmental Thresholds and Guidelines Manual does not
19 address ground-borne vibration. Caltrans has published a Transportation- and
20 Construction-Induced Vibration Guidance Manual, which provides criteria for
21 allowable vibration in terms of potential annoyance to people, as well as
22 potential damage to buildings. Based on the guidelines listed by Caltrans, the
23 most conservative thresholds for continuous sources such as construction
24 equipment and solid waste handling operations, expressed as the peak particle
25 velocity (PPV) that should not be exceeded, are as follows:

26 Guideline for vibration damage to buildings: 0.08 inches/second

27 Guideline for annoyance to people: 0.01 inches/second

28 **CalRecycle**

29 The Program EIR prepared for Statewide Anaerobic Digester Facilities
30 recommends using a sliding scale based on pre-existing noise levels developed
31 by the Federal Interagency Committee on Noise (1992). The criteria defining a
32 “substantial increase” for noise exposure, as presented in the Program EIR are
33 as follows:

34 For existing Ldn < 60 dBA: +5.0 dBA or more

35 For existing Ldn 60–65 dBA: +3.0 dBA or more

36 For existing Ldn > 65 dBA: +1.5 dBA or more

37

1 4.7.2.2 Approved Tajiguas Landfill Expansion Project

2 01-EIR-05 for the Tajiguas Landfill Expansion Project (see Section 3.9.3)
3 identified the following noise impacts for the approved Front Canyon
4 Expansion:

- 5 1. Short-term noise associated with construction of a new scale-house and
6 maintenance shop was considered a less than significant impact (Class
7 III). However, mitigation measure N-1 (maintenance of landfill
8 equipment) was adopted to reduce noise levels from landfill equipment.
- 9 2. Noise levels at the Arroyo Quemada community associated with
10 expanded landfill operations were considered a less than significant
11 impact (Class III). However, mitigation measure N-1 was adopted to
12 reduce noise levels from landfill equipment.
- 13 3. Noise levels at residences at Baron Ranch associated with expanded
14 landfill operations were considered a less than significant impact (Class
15 III). However, mitigation measure N-1 was adopted to reduce noise
16 levels from landfill equipment.
- 17 4. Noise levels associated with blasting of the north and west borrow areas
18 at nearby sensitive receptors were also considered a less than
19 significant impact (Class III). However, mitigation measure N-2
20 (limitations on the hours when blasting can occur, 8:00 am to 4:00 pm,
21 Monday through Friday) was adopted to further reduce impacts from
22 blasting events.
- 23 5. Noise levels associated with closure and post-closure activities was
24 considered a less than significant impact (Class III). However,
25 mitigation measure N-1 was adopted to reduce noise levels from landfill
26 equipment.

27 4.7.2.3 Approved Tajiguas Landfill Reconfiguration and Baron Ranch Restoration
28 Project

29 The Subsequent EIR for the Tajiguas Landfill Reconfiguration and Baron Ranch
30 Restoration Project estimated landfill operations noise by assuming the worst
31 case scenario consisting of several pieces of heavy equipment operating along
32 the perimeter of the disturbance limits of the landfill. Under this scenario, the
33 65 dBA CNEL contour was estimated to extend 420 feet beyond the
34 disturbance limits and noise impacts were determined to be adverse but less
35 than significant.

1 4.7.2.4 Proposed Tajiguas Resource Recovery Project

2 **Methodology and Assumptions**

3 The analysis of noise impacts is focused on noise-sensitive land uses that
4 include five residential locations (see Figure 4.7-1) in the vicinity of the existing
5 Tajiguas Landfill. Recreational uses occur on the neighboring Baron Ranch
6 and Arroyo Hondo, but these uses are not considered to be noise-sensitive.
7 The five locations were the same as identified in the Subsequent EIR for the
8 Tajiguas Landfill Reconfiguration and Baron Ranch Restoration Project. Since
9 the proposed project would be located entirely within the area of existing landfill
10 operations, it is reasonable to address these same residential receiver
11 locations.

12 For traffic noise levels along U.S. Highway 101, updated 65 Ldn noise contours
13 were developed using current traffic counts and truck traffic estimates from
14 Caltrans, using the FHWA Traffic Noise Model (TNM version 2.5). TNM 2.5
15 was used to determine the hourly Leq values for daytime and nighttime periods,
16 which were then combined to compute Ldn values. Traffic noise levels on U.S.
17 Highway 101 were estimated based on traffic volume data collected in
18 December 2012 and January 2013 (see Appendix K), which includes the
19 existing landfill truck traffic. Noise level changes due to the proposed project
20 were assessed by adding project-related trips (see trip generation in Table 4.9-
21 10) to current traffic volumes. Cumulative noise level changes due to the
22 proposed project were assessed by adding project-related trips to forecast year
23 2036 traffic volumes. Traffic volumes associated with the *CSSR Option* were
24 also included in the analysis.

25 For equipment operations, source noise values used in the analysis were taken
26 from a combination of measurements performed at solid waste handling
27 facilities, literature values for typical heavy construction equipment from the
28 FHWA Roadway Construction Noise Model (FHWA, 2006), or from other
29 sources. The approach to the noise analysis involved three steps:

- 30 1. Determine a composite source noise value for operating equipment at
31 each of the proposed facility locations; MRF, AD Facility, composting
32 area and energy facility;
- 33 2. Compute the CNEL value at the reference distance for each facility,
34 based on the proposed hours of operation, and compute the distance to
35 the 65 dBA CNEL contour; and
- 36 3. Compare the resulting CNEL values with those from the 2009 SEIR, and
37 make adjustments as appropriate to determine if any existing or likely
38 future residential areas would be affected by the new 65 dBA CNEL
39 contour.

1 Note that noise impacts associated with the relocated landfill maintenance
2 building were not specifically assessed as landfill equipment maintenance
3 activities are part of the environmental baseline, and the project would result in
4 moving this facility further from noise-sensitive land uses.

5 For ground-borne vibration, the preliminary estimating procedure from the
6 Caltrans Transportation- and Construction-Induced Vibration Guidance Manual
7 was used to estimate the PPV values at each residential location resulting from
8 equipment operation at each of the project facilities.

9 Throughout the analyses, two assumptions were used to assure a worst case
10 approach and for the sake of simplicity. These assumptions include:

- 11 • No attenuation in noise levels due to intervening topography, whether
12 natural (ridgelines between some residential locations and the project
13 site) or man-made (perimeter berms around the landfill disturbance area).
14 Under the right conditions, topographic barriers can provide a 5–10 dBA
15 reduction in noise levels, and major ridgelines can provide much greater
16 reduction. Along U.S. Highway 101, some residential receiver locations
17 are exposed more or less directly to the highway, so no topographic
18 reduction should be assumed. At other locations, however, homes are
19 located at an elevation well below that of the highway (such as in the
20 Arroyo Quemada community). Intervening ridgelines also separate most
21 of the residential receiver locations from proposed noise sources.
- 22 • No attenuation in noise levels from the MRF or the AD Facility due to their
23 building enclosures. These facilities would be enclosed within metal
24 buildings, which if completely covering the noise sources would provide
25 measurable noise reduction. However, since both buildings would have
26 large openings for trucks and heavy equipment to enter and exit, the
27 effective noise reduction from these building shells would be substantially
28 reduced. For purposes of this analysis, it is conservatively assumed that
29 such access doors are open and convey noise emissions without any
30 reduction associated with the facility enclosure.

31 With respect to project design, no unique or special aspects were assumed
32 beyond those included in the project description (Section 3.5). Based on
33 information provided by the proposed vendor, the Energy Facility would include
34 reinforced concrete walls, insulated metal roof, engine exhaust silencers and
35 acoustical gaskets on the doors.

36

Impact TRRP N-1: Project-related construction could generate short-term noise that would result in an adverse but less than significant impact on noise-sensitive receptors on adjacent agriculturally zoned land – Class III Impact.

Construction of the proposed project would include use of heavy-duty trucks and equipment at the MRF/AD Facility site (current landfill operations deck), proposed composting area, proposed maintenance building site, proposed water tanks site and proposed composting area run-off collection tank site. Each of these areas are located at least 1,600 feet from the nearest noise-sensitive land use (planned Hart residence), which would not be significantly impacted by construction noise (see County threshold e.).

Landfill operations trailers would be temporarily relocated to either a location northeast of the landfill top deck or on a deck southeast of the green waste operations deck within 800 feet of the planned Hart residence during construction of the project facilities. However, noise associated with re-locating landfill operations would involve installing pre-fabricated trailers and moving existing intermodal containers rather than constructing new buildings. These activities would be limited to less than a month, and would be limited to the existing permitted landfill operating hours. Overall, construction noise impacts would be less than significant.

Impact TRRP N-2: Project-related vehicle traffic on U.S. Highway 101 would result in an adverse but less than significant increase in noise levels at noise-sensitive receptors near the landfill – Class III Impact.

Project-related traffic increases would be minimal as compared to existing traffic on U.S. Highway 101, and result in noise increases at nearby residential land uses of less than 0.1 dBA CNEL (see Table 4.7-1). Project-related noise would not result in new exceedances of the 65 dBA CNEL threshold, or cause noise increases of 1.5 dBA or more. Therefore, traffic noise impacts are considered less than significant.

Table 4.7-1. Summary of U.S. Highway 101 Traffic Noise Impacts

Receiver	Daytime (dBA Leq)		Nighttime (dBA Leq)		Daily (dBA CNEL)	
	2013	2013 + Project	2013	2013 + Project	2013	2013 + Project
Arroyo Hondo residence	63.1	63.1	57.8	57.8	66.1	66.1
Arroyo Quemada community	67.3	67.3	62.0	62.0	70.3	70.3
Baron Ranch residence	61.0	61.0	55.7	55.7	64.0	64.0
Calle Real residences	68.7	68.7	63.4	63.4	71.7	71.7
Hart residence (planned)	61.3	61.3	55.8	55.9	64.2	64.2

1 **Impact TRRP N-3: Noise associated with operation of project facilities**
2 **would result in an adverse but less than significant impact on noise-**
3 **sensitive land uses near the landfill – Class III Impact.**

4 Noise would be generated from many of the project facilities, including the MRF
5 (sorting equipment, mobile equipment), the AD Facility (mobile equipment,
6 screening equipment), the composting area (mobile equipment, grinder), and
7 from the energy facility (CHP engines). Composite reference noise levels were
8 developed for each major project facility (see Tables 4.7-2 through 4.7-6).
9 Noise levels were estimated for each facility at each noise-sensitive receiver,
10 based on the respective operating hours for each facility. The resulting noise
11 levels were then combined to produce a 65 dBA CNEL noise contour (see
12 Figure 4.7-1), and a combined noise level at each noise-sensitive receiver (see
13 Table 4.7-7).

14 These combined noise levels are conservatively high since they do not account
15 for any noise reduction due to intervening topography between project facilities
16 and noise-sensitive receptors. As shown in Table 4.7-7, noise levels at
17 sensitive receptors are projected to be below 65 dBA CNEL criteria and the
18 resulting increase above existing landfill operations noise is projected to be no
19 greater than 1 to 2 dBA. Project-related operations noise would result in a less
20 than significant noise impact.

21 **Impact TRRP N-4: Vibration associated with operation of project facilities**
22 **would result in an adverse but less than significant impact on residential**
23 **land uses near the landfill – Class III Impact.**

24 The ground-borne vibration assessment is based on the vibration effects from
25 mobile equipment. As a worst-case scenario, it was assumed a large bulldozer
26 would be operating at each of the project facility sites. The procedure
27 described by the Caltrans Vibration Guidance Manual was used (Caltrans,
28 2004) to estimate vibration levels. The reference source vibration for a large
29 bulldozer is a peak particle velocity (PPV) of 0.089 in/sec at a distance of 25
30 feet (Federal Transit Administration, 2006). Table 4.7-8 provides the results of
31 the vibration assessment at residential receivers for each project facility.
32 Project-related vibration would not exceed the 0.01 inches/second threshold for
33 human annoyance and would be well below the 0.08 threshold for building
34 damage, therefore project generated vibration impacts would not be significant.

1

Table 4.7-2. Reference Noise Levels for Proposed MRF Equipment

Equipment/Vehicle Type (Rated Engine power)	Quantity	Usage Factor	Lmax (dBA)	Leq (dBA)	Reference Distance (ft.)	References and/or Assumptions
Caterpillar 980M Volvo L440G ² wheeled loader (386 260 hp)	2	40%	80	79	50	RCNM (FHWA, 2006): Table 1 (front-end loader)
Caterpillar 938K Volvo L90G ² wheeled loader (169 473 hp)	1	40%	80	76	50	RCNM (FHWA, 2006): Table 1 (front-end loader)
“Volvo L20F” wheeled loader (56 hp)	4	40%	80	76	50	RCNM (FHWA, 2006): Table 1 (front-end loader)
Caterpillar M322D material handler (173 hp)	1	40%	85	81	50	RCNM (FHWA, 2006): Table 1 (excavator)
Caterpillar 2P-6000 Toyota Forklift (61 57 hp)	3	40%	80	81	50	Est. similar to wheeled loader
Tractors – Freightliner	(Counted as heavy truck along Access Road in traffic noise analysis.)					
Trailers – Western	(Counted as heavy truck along Access Road in traffic noise analysis.)					
Trailers – End Dump	(Counted as heavy truck along Access Road in traffic noise analysis.)					
Utility truck and trailer (470 hp)	1	40%	84	80	50	RCNM (FHWA, 2006): Table 1 (flatbed truck)
Pick-up trucks (250 hp)	2	40%	75	74	50	RCNM (FHWA, 2006): Table 1 (pick- up truck)
Truck hydraulic pumps	1	10%	73	63	50	Azusa MRF & TS (RBF Consulting, 2011)
Truck air brake	1	1%	85	65	50	Azusa MRF & TS (RBF Consulting, 2011)
Conveyor	1	100%	65	65	50	Azusa MRF & TS (RBF Consulting, 2011)
Alarms	1	10%	82	72	50	Azusa MRF & TS (RBF Consulting, 2011)
Voices	1	100%	62	62	50	Azusa MRF & TS (RBF Consulting, 2011)
Sorting	1	100%	68	68	50	Azusa MRF & TS (RBF Consulting, 2011)
Shredder	1	50%	76	73	50	SCRTS ND/IS (Fugro West, 1995)
Compactor-baler	1	10%	87	77	50	SCRTS ND/IS (Fugro West, 1995)
Rolling bed dryer	1	100%	-	85	50	Vendor data sheet
Logarithmic Sum of Equipment/Vehicle Noise for MRF:				<u>91.0</u> 88.2	50	(CNEL = 92.2 90.0)* *based on operation hours, and nighttime background of 43 dBA

2

3

1 **Table 4.7-3. Reference Noise Levels for Proposed AD Facility Equipment**

Equipment/Vehicle Type (rated engine power)	Quantity	Usage Factor	Lmax (dBA)	Leq (dBA)	Reference distance (ft.)	References and/or assumptions
Caterpillar 938M "Volvo L110G" wheeled loader (169 260 hp)	≥ 4	40%	80	76	50	RCNM (FHWA, 2006): Table 1 (front-end loader)
Screening, electric (Titech)	1	50%	85	82	50	RCNM (FHWA, 2006): Table 1 (vibrating hopper)
Tennant M30 scrubber-sweeper	1	25%	85	75	50	RCNM (FHWA, 2006)
Logarithmic Sum of Equipment/Vehicle Noise for AD Facility:				84.3 83.0	50	(CNEL = 80.0 84.1)* *based on 7 a.m. – 4 p.m. equipment operating hours, and nighttime background of 43 dBA

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3 **Table 4.7-4. Reference Noise Levels for Proposed Composting Area Equipment**

Equipment/Vehicle Type (Rated Engine Power)	Quantity	Usage Factor	Lmax (dBA)	Leq (dBA)	Reference Distance (ft.)	References and/or Assumptions
"Screen machine 612T" tracked trammel screen (84 hp)	1	50%	85	82	50	RCNM (FHWA, 2006): Table 1 (vibrating hopper)
Caterpillar 938K "Volvo L90G" wheeled loader (169 473 hp)	1	40%	80	76	50	RCNM (FHWA, 2006): Table 1 (front-end loader)
"Vermeer CT 1010" windrow turner (215 hp)	1	50%	75	72	50	RCNM (FHWA, 2006): Table 1 (tractor)
"Morbark 3800" horizontal grinder (electric, 1,200 hp)	1	20%	89	82	50	Padre Associates, Santa Barbara County 2008:4)
Logarithmic Sum of Equipment/Vehicle Noise for the Composting Area:				85.7	50	(CNEL = 82.7)* *based on operation hours, and nighttime background of 43 dBA

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1 **Table 4.7-5. Reference Noise Levels for the Energy Facility – Mechanical Radiation**

Mechanical Casing Radiated Noise ¹	Unweighted dB	A-weighting adjustment	dBA	Building Noise Reduction (dB) ²	dBA at 1m from Building Surface
31.5	84	-39.4	44.6	13	32
63	88	-26.2	61.8	17	45
125	97	-16.1	80.9	22	58
250	95	-8.6	86.4	22	64
500	93	-3.2	89.8	27	63
1,000	88	0	88	34	54
2,000	87	1.2	88.2	39	49
4,000	90	1	91	35	56
8,000	88	-1.1	86.9	32	55
Logarithmic Sum:			97 dBA		68 dBA

¹ Octave band center frequency (hertz)

² Based on 6"-thick, 49 lb/sf painted concrete wall (or comparable) and small (<=0.5% of façade area) vent opening; with a closed 8' tall by 7' total width double-door (STC-30) in the south wall

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Table 4.7-6. Reference Noise Levels for the Energy Facility – Exhaust

Combustion Exhaust Noise ¹	Unweighted dB	A-weighting adjustment	dBA	Silencer Noise Reduction (dB)	Attenuated Exhaust at 1m (dBA)
31.5	105	-39.4	65.6	12	54
63	120	-26.2	93.8	22	72
125	127	-16.1	110.9	40	71
250	115	-8.6	106.4	45	61
500	113	-3.2	109.8	42	68
1,000	111	0	111	40	71
2,000	108	1.2	109.2	40	69
4,000	109	1	110	40	70
8,000	107	-1.1	105.9	40	66
Logarithmic Sum:			118 dBA		78 dBA

¹ Octave band center frequency (hertz)

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Table 4.7-7. Summary of Operational Noise Impacts (dBA CNEL)

Receiver	MRF	AD Facility	Energy Facility	Composting Area	Existing Operations	Sum
Arroyo Hondo residence	55 53	43 47	28	43	57	59
Arroyo Quemada community	53 54	41 45	26	45	58	59
Baron Ranch residence	52 50	40 44	25	45	57	58
Calle Real residences	47 45	35 39	20	39	53	54
Hart residence (planned)	57 55	45 49	30	51	64	65 64

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Table 4.7-8. Summary of Vibration Impacts (PPV inches/second)

Receiver	MRF	AD Facility	Composting Area	Existing Operations
Arroyo Hondo residence	0.000369	0.000385	0.000270	0.000477
Arroyo Quemada community	0.000289	0.000300	0.000364	0.000646
Baron Ranch residence	0.000250	0.000254	0.000370	0.000562
Calle Real residences	0.000138	0.000139	0.000167	0.000203
Hart residence (planned)	0.000477	0.000500	0.000726	0.002699

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Relocated Landfill Facilities

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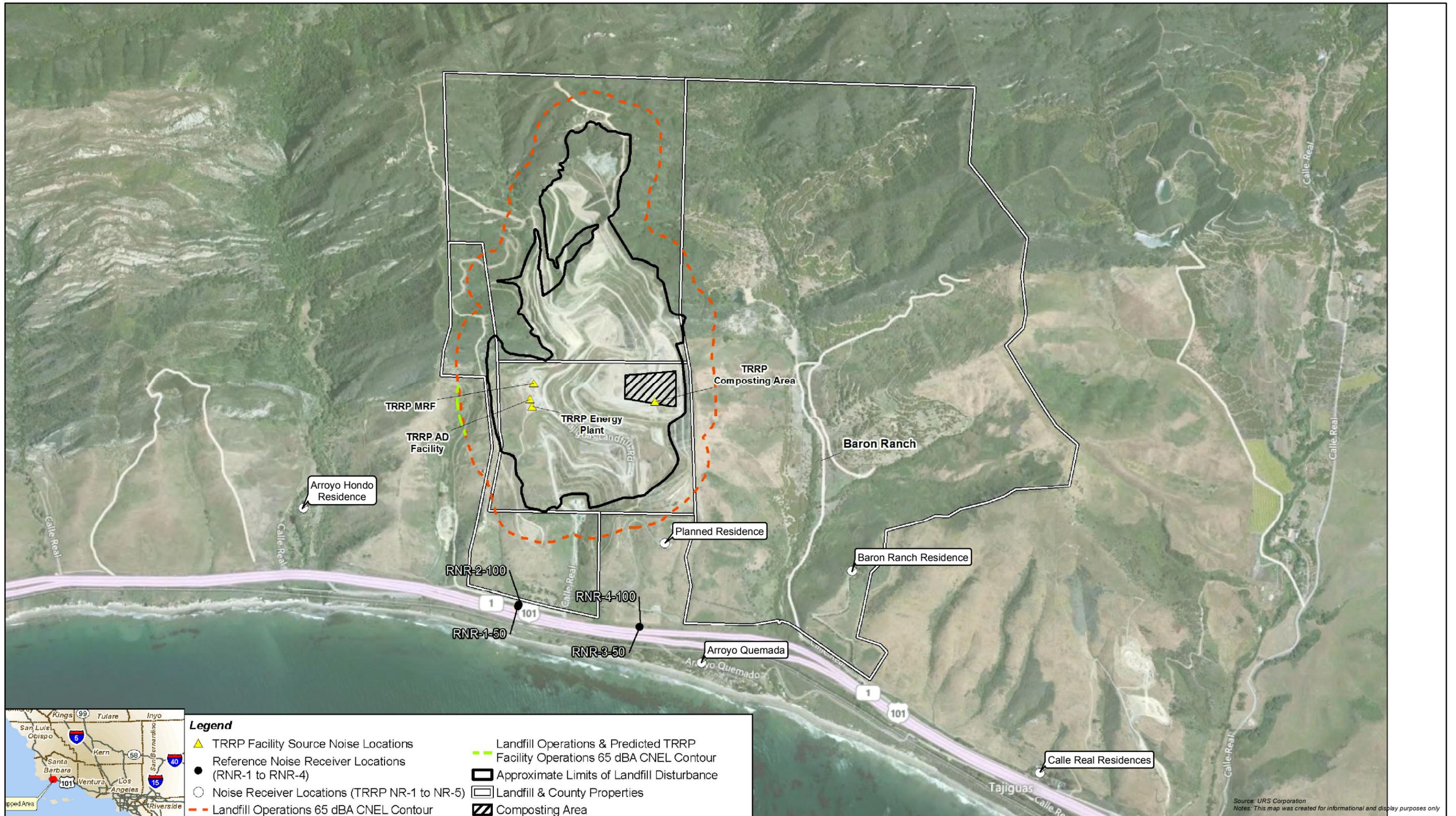
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Operations facilities (primarily portable offices) may be temporarily relocated during the project construction period to an area north of the landfill top deck or to the southern portion of the landfill. Landfill equipment maintenance facilities would be relocated to the area north of the landfill top deck (see Figure 3-4). These facilities are existing and part of the environmental baseline. However, the proposed project may result in temporarily moving the operations facilities to within 800 feet of the planned Hart residence. However, noise generation would be limited to light vehicle traffic during daylight hours and would not exceed the County's 65 dBA CNEL noise threshold at the nearest noise-sensitive use. The maintenance facilities would be relocated to the back canyon and not in proximity to any noise receivers. Overall, noise impacts associated with relocated landfill facilities would be less than significant.



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Back of Figure 4.7-1

1 4.7.2.5 Proposed Tajiguas Resource Recovery Project with Optional Comingled
2 Source Separated Recyclables (CSSR) Component

3 Inclusion of the *CSSR Option* would require additional sorting facilities within
4 the proposed MRF building (see Figure 3-8). The addition of these facilities
5 and the 10,000 sf of additional building area would have an indiscernible effect
6 on the equipment noise and duration of construction of the MRF, and would not
7 alter the significance of construction noise impacts.

8 The small amount of additional vehicle traffic (40 ADT) associated with the
9 *CSSR Option* would not increase traffic noise levels along U.S. Highway 101.
10 Project-related noise with the *CSSR Option* would not result in new
11 exceedances of the 65 dBA CNEL threshold, or cause noise increases of 1.5
12 dBA or more. Therefore, traffic noise impacts are considered less than
13 significant.

14 The very small amount of additional activity and equipment associated with the
15 *CSSR Option* would not substantially increase operational noise levels provided
16 in Table 4.7-7. Project-related operations noise with the *CSSR Option* would
17 result in a less than significant noise impact.

18 The very small amount of additional activity associated with the *CSSR Option*
19 would not substantially increase vibration levels provided in Table 4.7-8 and
20 impacts would remain less than significant.

21 4.7.2.6 Extension of Landfill Life Impacts

22 **Impact TRRP N-5: Project-related extension of the life of the Tajiguas**
23 **Landfill would extend adverse but less than significant landfill operational**
24 **noise impacts further in time – Class III Impact.**

25 As discussed in Section 3.4, project-related diversion of recyclable material and
26 organic waste is anticipated to extend the life of the Tajiguas Landfill by about
27 10 years. The combined effect of continued landfill operations and operation of
28 the project facilities on project area noise levels is discussed in Section 4.7.2.4.
29 Separately, prior environmental documents prepared for the Tajiguas Landfill
30 determined that noise impacts associated with landfill operations were less than
31 significant (see Sections 4.7.2.2 and 4.7.2.3). These analyses were based on
32 presumed operation of equipment simultaneously along the entire landfill
33 perimeter. However, by the time the proposed project is operational, residual
34 waste disposal activities would occur in the back canyon area of the landfill
35 property, which would increase the distance from this existing noise source to
36 surrounding noise-sensitive receptors. In addition, diversion of MSW
37 associated with the proposed project would reduce the volume of waste and
38 associated equipment required for disposal. Therefore, with implementation of
39 the proposed project, less than significant noise impacts associated with landfill
40 operations (see Section 4.7.2.2) could continue further in time as compared to
41 earlier closure of the landfill in the absence of the proposed project.

4.7.2.7 Decommissioning Impacts

Impact TRRP N-6: Heavy equipment and vehicles used during decommissioning would generate noise that may affect noise-sensitive receptors near the landfill – Class III Impact.

Similar to project construction activities (see Impact TRRP N-1), the use of heavy equipment and vehicles to dismantle and remove project facilities would generate noise. However, the intensity and total amount of decommissioning activity would be less than associated with construction, decommissioning would occurring during daytime hours, and all activity would occur at least 1,600 feet from the nearest existing noise-sensitive land use. Based on the Gaviota Coast Plan, adjacent land uses would remain in agriculture, such that no new noise-sensitive land uses are anticipated to be constructed near the Landfill. Therefore, noise impacts during decommissioning are considered less than significant.

4.7.2.8 Cumulative Impacts of the Tajiguas Resource Recovery Project

Impact TRRP N-CUM-1: Future (2036) traffic on U.S. Highway 101 associated with forecast growth combined with project-related vehicle traffic could contribute to an adverse but less than significant cumulative increase in noise levels along the highway corridor - Class III Cumulative Impact; Project Contribution – Not Considerable (Class III).

By 2036, noise levels along U.S. Highway 101 are expected to increase by about 0.6 dBA at most locations. Project-related traffic increases would be minimal as compared to year 2036 traffic (forecasted growth) on U.S. Highway 101, and result in noise increases at nearby residential land uses of less than 0.1 dBA CNEL (see Table 4.7-9). Forecasted growth combined with project-related noise would not result in new exceedances of the 65 dBA CNEL threshold, or cause noise increases of 1.5 dBA or more. Therefore, cumulative U.S. Highway 101 traffic noise impacts would be less than significant and the project’s incremental contribution would not be cumulatively considerable. The very small amount of additional vehicle traffic associated with the *CSSR Option* would not increase cumulative noise levels provided in Table 4.7-9 and would also not be cumulatively considerable.

Table 4.7-9. Summary of U.S. Highway 101 Cumulative Traffic Noise Impacts

Receiver	Daytime (dBA Leq)		Nighttime (dBA Leq)		Daily (dBA CNEL)	
	2036	2036 + Project	2036	2036 + Project	2036	2036 + Project
Arroyo Hondo residence	63.7	63.7	58.4	58.4	66.7	66.7
Arroyo Quemada community	67.9	67.9	62.6	62.6	70.9	70.9
Baron Ranch residence	61.6	61.6	56.3	56.3	64.6	64.6
Calle Real residences	69.3	69.3	64.0	64.0	72.3	72.3
Hart residence (planned)	61.8	61.9	56.4	56.4	64.8	64.8

1 **Impact TRRP N-CUM-2: Noise associated with construction and operation**
2 **of project facilities combined with noise generated by other cumulative**
3 **projects would result in adverse but less than significant noise levels at**
4 **noise-sensitive land uses near the landfill property – Class III Cumulative**
5 **Impact; Project Contribution – Not Considerable (Class III).**

6 Only three of the cumulative projects (see Section 3.6) are located within 2
7 miles of the landfill site: Bean Blossom residences – Lot H and Lot X
8 (construction of these residences has been completed), Shell/Hercules
9 Remediation and Slope Stabilization, and Simon Residence. Construction-
10 related noise from these other projects may adversely affect the ambient noise
11 environment of the area. However, construction noise would be temporary in
12 nature, and would be virtually undetectable over the dominant noise source in
13 the area (U.S. Highway 101).

14 Operational noise (vehicles, landscape maintenance, music, etc.) generated by
15 the three residences may adversely affect the ambient noise environment of the
16 area, but would be virtually undetectable over the dominant noise source in the
17 area (U.S. Highway 101).

18 The Shell/Hercules Remediation project, ~~for which a Remedial Action Plan is~~
19 ~~under review and due to be amended in 2014, may~~ would involve ongoing
20 construction-like activity and may adversely affect the ambient noise
21 environment of the area. ~~However, details regarding the are not known at this~~
22 ~~time.~~ Given the dominance of U.S. Highway 101 noise and the fact that the
23 remediation site and the landfill site are both within canyons separated by a
24 ridge, noise levels would not be additive and significant cumulative noise
25 impacts to residences in the area are not expected.

26 Overall, cumulative noise levels are unlikely to exceed the 65 dBA CNEL
27 threshold at noise-sensitive receivers and therefore noise impacts would not be
28 significant. The incremental contribution of the proposed project to cumulative
29 noise impacts would not be cumulatively considerable.